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Investigation on Enhancing Heat Transfer Properties Experimentally Using Grooved Tube

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Abstract: One of the many applications in industry is heat transfer in pipe flow. Heat exchangers are one of the most often utilized applications among the many that are used in industry. Heat exchangers work on the premise of transferring heat without requiring physical contact between two fluids of different temperatures. Heat transfer increase is essential for industry energy and material resource conservation. Compact heat exchangers with good performance and low weight are needed in the industry due to energy and material conservation. The heat transfer business effectively uses improved surfaces to obtain more compact and efficient units. These days, thanks to straightforward construction and efficient heat transmission improvement.

Keywords: Thermal performance; Grooves Tubes; Forced Convection, Heat transfer coefficient.

1. Introduction

The two techniques utilized to improve heat transfer are the active and passive approaches. While working fluid additives and various surface geometries are needed for the passive approach, external sources are needed for the active method. Numerous experimental and numerical investigations were conducted to determine the significance of the heat transfer increase. The primary goal of this activity is to deliver material, financial, and energy savings for users of heat transfer improvement technologies by creating more efficient heat exchangers and thermal heat transport devices for industrial and other applications. These days, modern heat exchangers primarily use grooved tubes because of their efficacious heat transfer increase capabilities.

Modern high-efficiency air conditioning and refrigeration systems rely heavily on micro-grooved tubes. These tubes typically contain grooves around the inner walls that are roughly 0.2 mm deep and have a pitch of 0.5 mm. The grooves can be arranged in different designs. These days, tubes with crosshatched, herringbone, axial, and helical patterns are available. Previous research has led us to believe that micro grooved tubes can lead to improved heat transfer coefficients with a little higher-pressure loss when compared to smooth tubes. At low mass flows, this effect is more pronounced. Micro grooved tubes are used in air conditioning and cooling system condensers/evaporators and coolers. These tubes combine smaller heat exchangers with increased efficiency. Consequently, The main aim of the present research work is to investigate the effect on heat transfer performance of the modified surface (helically grooved) of the tube on the enhancement in heat transfer. The prospect of using the helically grooved tube is for reducing the thickness of the boundary layer which is focused at better fluid mixing near the tube wall caused by the secondary flows from the wall to the core flow. Transfer of heat from one place to another due to temperature difference is known as heat transfer and those devices which is used to transfer heat are known as heat exchangers. These are the most common thermal equipment in large industries and manufacturing processes which are employed for the heat transfer, heat extraction and heat energy re-generation according to the space and time of the industries and manufacturing plants. Due to the considerations of the space, material cost and global economy various method for heat transfer enhancement are being developed. All these methods of heat transfer enhancement can be mainly classified into two major group, namely: active techniques and passive techniques. Active techniques make the utilization of external power for the heat transfer enhancement heat exchanger while in contrast passive techniques uses no direct power for the heat transfer enhancement. Each of these methods of heat transfer enhancement are effective according to the condition and mode of heat of transfer. Generally, heat transfer depends on the material property like thermal conductivity, fluid property like

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convection heat transfer coefficient, exposed surface area, velocity of fluid movement etc, which are considered constant for a specific case. Properties of heat transfer material and fluid cannot be changed but surface area and the speed of fluid can be altered for the same setup to enhance the efficiency of Heat Exchangers. In comparison with the plain tube, internal spiral groove imparts swirl motion to the axial flow in the near region

2. Literature Review

Kadir *et al.* worked on the enhancement of convective heat transfer in a single-phase turbulent flow by using helically grooved tubes. In the evaluation, the isothermal friction and thermal performance factor is calculated under the effects of pitch-to-diameter ratio and rib-height to diameter ratio of helically grooved tubes on the heat transfer enhancement. After studying for the turbulent flow, results shows that the thermal performance and the heat transfer characteristic of the grooved tube are increased in comparison with plane tube.

Jacqueline Biancon Copetti *et al.* have studied heat transfer characteristics and friction characteristics for single-phase flow (water) in micro-grooved tubes. The performance analysis with a 4.76 mm radius micro-fin tube for thermal and hydraulic behavior under the laminar and turbulent flow was carried out experimentally. In the heating tests, different operational conditions were considered. The pressure drop and flow rate, inlet and outlet temperatures and various wall temperatures along the tube, were measured. The higher heat transfer performance shows by micro-grooved tube than the smooth tube. About 80% increment shows in heat transfer coefficient.

Takahiro Adachi *et al.* studied correlation between pressure drop in channels with periodically grooved parts and heat transfer along the stream wise direction is investigated for different channels configurations by considering fully developed flow. Heat transfer isimproved after the divergence with enhancement of pressure drop. Efficiency defined as ratio of heat transfer enhancement to the pressure drop enhancement. It is seen that the channels with expanded grooves perform efficiently, while the channels with contracted groove inefficient.

M. Greiner *et al.* have studied direct numerical simulations of 3D flow and enhanced convection in a channel with transverse, symmetric grooves in two opposite walls are performed using the spectral element technique. The flow is driven by constant pressure gradient. Results are presented for Reynolds no. range 180<Re<1175. A series of flow transitions is observed as the Reynolds number is increased, from steady two-dimensional flow, to traveling two arid three-dimensional wave structures, and finally to the three-dimensional mixing. Periodic ejection of slow moving fluid from the grooves causes significant flow rate unsteadiness. Three-dimensional simulations predict friction factor and Nusselt number values to within 20% of measured values over the narrow Reynolds number range where overlapping data exists. Two-dimensional simulations are found to be inadequate to transport in this channel for Re > 400.

I.S.Park, *et al.* have developed a 3D heat transfer characteristics analysis procedure for the coupled evaporating/condensing films going down along the inner/outer walls of vertical grooved tube has developed. The analysis is successful in results the freelocation of surface along with the amount of condensate and another major 3D characteristic.

Most of the condensation is observed to take place on bare place of groove surface and shows that how the heat transfer characteristics are improved by grooved surface. The results are indicated for various groove densities and operating condition. The optimum groove number looks to vary with the temperature difference of two sides. The effect of surface tensions also discussed.

3. Development of experimental Set up

The experimental setup generally consists of three part; the test section, air supply unit with necessary adoption and measuring devices. The air supply unit and its accessories consist of a blower, flow controlvalves, orifice meter, inclined tube differential manometer and grooved tubes. Heater is mounted on the grooved tube and space between them is filled withthe silicon paste to transfer the uniform heat to the tube. Arrangement has been made to vary heat input by connecting the band heater through the dimmerstat to main supply. The amount of electrical energy supplied to heater can be measured by connecting the voltmeter and ammeter in between heater. The flow control valve has been connected at the downstream of the tube to vary the flow. The schematic arrangement of the experimental set up is as shown in figure 1.

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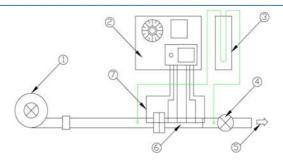


Fig.1 Schematic layout experimental setup.

1) Blower, 2) Control Panel, 3) Manometer, 4) Control Valve, 5) Air Flow, 6) Test Section, 7) Temperature Sensor

3.1 Test Tubes

The test section is as mentioned above consist of two different grooved tubes, its specifications as follows

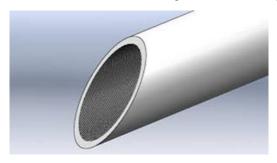


Fig.2 Test Section- Grooved Tubes

- 1. Tube material: Copper
- 2. Outside Diameter: -31.0 mm
- 3. Tube Thickness:-1 mm
- 4. Tube Length: 2 feet
- 5. Grooved per feet :- 12/20
- 6. Set 1 Grooved per feet = 12
- 7. Set 2 Grooved per feet = 20

3.2 Test Methodology

- 1. Make sure that connections of the thermocoupleare properly attached with the surfaces whose temperature is to be measured.
- 2. Switch on the Heater input and Centrifugal Blowerinput.
- 3. Using rheostat increase the supplied air heaterinput.
- 4. Start taking readings with time, set as zero
- 5. The blower is started and mass flow rate of air is adjusted as per requirement with the help of gate valve to have turbulent flow.
- 6. The mass flow rate of air is measured with the helpof orifice meter.
- 7. Pressure difference between outlet and inlet side of the orifice meter is recorded with the help of U- Tube Manometer and attached scale.
- 8. Before taking the readings the steady state condition is maintained. Initially the readings on plain tube and then for grooved tube alone were taken. This is to validate and compare the performance of grooved tube with plain tube.
- 9. The temperature readings Ti (Ambient temperature), T7 (Air temperature at inlet side), T8 (Air temperature at outlet side), and T1 to T6 (temperatures at different location in test section) were recorded with the help of multimeter present with the apparatus.

Experimental Evaluation of thermal performance characteristics is carried out by varying the heat input from 25 W to 100 W in the step of 25 W. Readings are taken at steady state. Heater is placed between two testplates.

Whole test set up is mounted vertically. Voltage supplied is varied with the help of Variac dimmerstat. 3.3 Test Parameters and Calculations

Experimentation was performed on the circular pipe atvarious pitches of grooved tubes.

Table 3.1 Test parameters

Parameter	Description
Heat load (W)	25W,50W,75W,100W
Time	To reach up to Steady State

All the required components were assembled and experimental setup was developed. The required instruments were attached at proper configuration and the setup is prepared for the experimentation.

Data Reduction

Heat Supplied (Q) = $V \times I$

Heat Transfer coefficient (hth) = Q/A (ΔTs - ΔTa)Discharge through orifice (q) = $CdAo\sqrt{2}gha$ Number (Nu) = $0.023Re^{0.8}pr^{0.4}$

Heat Transfer coefficient (h_{th}) = (Nu)/kL

4. Results and Discussion

The effect of grooves on tube on the heat transfer characteristics are presented in both terms of Nusselt number and heat transfer coefficient for plane tubes at the same Reynolds numbers. The Nusselt number and heat transfer coefficient is calculated by varying Reynolds number.

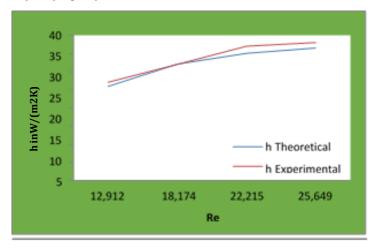


Fig.3 Comparison between of hth and hexp for plane tube

Heat transfer coefficient calculated by experimental method and theoretical method is similar for plane tube. From Figure no. 3, it can be said that experimental setup is validated.

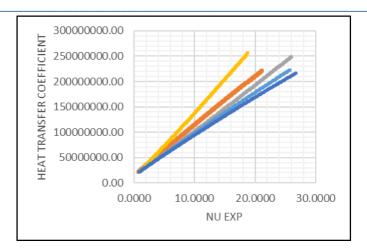


Fig.4Nusselts Number verses Heat transfer coefficientat 25W for different tubes

The above graph of heat input 25 Watt shows that grooved tubes shows increment in heat transfer coefficient. Set1 (Grooved pitch-12 per feet) shows 6.89% in comparison with plane tube. Set2 tube(Grooved pitch-20 per feet) shows 13.56% in comparison with plane tube.

The above graph of heat input 75 Watt shows that grooved tubes shows increment in Nusselt number. Set1 tube shows 6.47% in comparison with plane tube and Set2 tube shows 10.83% in comparison with plane tube.

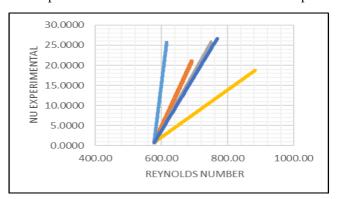


Fig.5 Reynolds Number verses Nusselt Number at 100W for different tubes

The above graph of heat input 100 Watt shows that grooved tubes shows increment in Nusselt number. Set1 tube shows 6.13% in comparison with plane tube and Set2 tube shows 10.55% in comparison with plane tube.

Conclusion

In this study forced convection heat transfer characteristics from grooved tube has been investigated experimentally. The effect of variation in pitch of grooved has been investigated with variation in mass flow rate of air and heat input to grooved tube. The whole experimentation has been carried out underturbulent flow condition. This investigation was carried out to observe if the use of grooves on tube can enhance heat transfer characteristics for turbulent flow.

The following conclusions were drawn from this study.

- For 25W, 50W, 75W and 100W, the enhancement in force convective heat transfer coefficient of set1 tube in compare with plane tube is observed as 6.89%, 4.48%, 6.49% and 6.13% respectively. For 25W, 50W, 75W and 100W, the enhancement in convective heat transfer coefficient of set2 tube in compare with plane tube is observed as 13.56%,11.30%, 10.84% and 10.55% respectively.
- For 25W, 50W, 75W and 100W, the enhancement in Nusselt number of set1 tube in compare with plane tube is observed as 6.89%, 4.50%, 6.47% and 6.13% respectively.
- For 25W, 50W, 75W and 100W, the enhancement in Nusselt number of set2 tube in compare with plane tube

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is observed as 13.54%, 11.52%, 10.83% and 10.55% respectively.

- Heat transfer enhancement under forced convection can be achieved by using grooved tubes. It is also observed that set 2 (20 pitch per feet) facilitates higher heat transfer augmentation when compared to the plane tube and set 1 (12 pitches per feet).
- Thus, the grooved on surface of the tube was found to enhance heat transfer over a plain tube surface for turbulent airflows.

References

- [1] KadirBilen, Murat Cetin, Hasan Gul, Tuba Balta, (2009), The Investigation of groove geometry effect for internally grooved tube, Applied Thermal Engineering 29, 753-76
- [2] Jacqueline Biancon Copetti, Mario Henrique Mecagnan, Daiana de Souza, Rejane De Cesaro Oliveski, (2004), Experiments with micro fin tube in single phase, International Journal of Refrigeration 27, 876-883.
- [3] Takahiro Adachi, Haruo Uehara, (2001), Correlation between heat transfer and pressure drop in channels with periodically grooved parts, International Journal of Heat and Mass Transfer 44, 4333-4343
- [4] M. Greiner, R. J. Faulker and R.A. Wirtz, (1997), Simulations of three-dimensional flow and Augmented Heat transfer in symmetrically grooved channel, Proceeding of Heat Transfer Division, Volume 3, 269-27
- [5] S. Park, D. H. Choi, (2001), Heat and Mass Transfer analysis for condensing film flow along a vertical grooved tube, International Journal of Heat and Mass Transfer 44, 4277-4285.